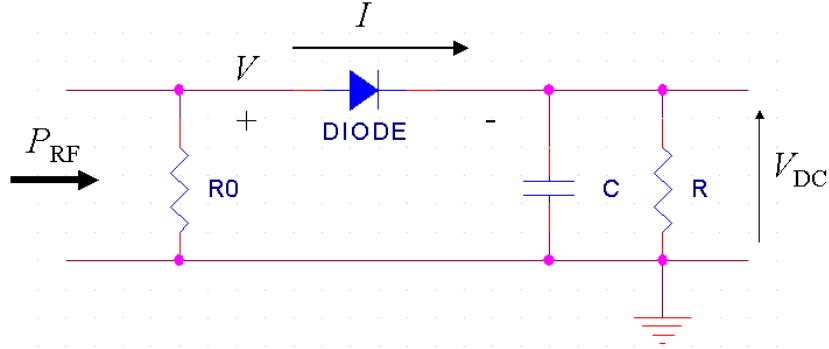


WORKING PRINCIPLE OF A DIODE POWER METER

A power meter should include a matching network, the non-linear element (diode), an output low-pass filter and the final load. We can consider the simplified circuit shown in figure, with an input matching impedance $R_0 = 50 \Omega$. The diode equation is:

$$I = I_s [\exp(V/nV_T) - 1], \quad (1)$$

where $V_T = kT/e \cong 25 \text{ mV}$ at ambient temperature, k is the Boltzmann constant, n a number between 1 and 2, T the absolute temperature value in K and I_s the inverse saturation current.



In order to describe the diode behavior for low voltages, we can develop in series the exponential:

$$I = I_s \left(\frac{V}{nV_T} + \frac{V^2}{2(nV_T)^2} + \frac{V^3}{3!(nV_T)^3} + \dots \right) \quad (2)$$

If we consider an input sinusoidal voltage V , due to the input power R_0 , with $V = V_{RF} \sin(\omega t)$ and thus $P_{RF} = \frac{V_{RF}^2}{2R_0}$ (at radiofrequency, the diode cathode is grounded by the capacitor C , therefore the whole RF voltage falls on the diode).

For very-low voltages $V \ll V_T$ we can stop the series to the second term, neglecting the contribution of the higher-order terms. In this approximation, the DC component of the current, equal to the average value of I is given by:

$$I_{DC} = \langle I \rangle = I_s \frac{\langle V^2 \rangle}{2(nV_T)^2} = I_s \frac{V_{RF}^2 \langle \sin^2(\omega t) \rangle}{2(nV_T)^2} = I_s \frac{V_{RF}^2}{4(nV_T)^2} \quad (3)$$

The differential resistance R_D of the diode is given by:

$$\frac{1}{R_D} = \left. \frac{\partial I}{\partial V} \right|_{I=0} = \frac{I_s}{nV_T} \quad (4)$$

For a RF diode, the saturation current has value close to $10 \mu\text{A}$, hence its differential resistance is equal to some $\text{k}\Omega$: being $R_D \gg R_0$, the diode presence does not compromise the input line matching. The current I_{DC} falls on the diode differential resistance R_D in parallel with the load R , whose value is $\gg R_D$. In this way we obtain an output DC voltage equal to:

$$V_{DC} = I_{DC} R_D = R_D I_s \frac{V_{RF}^2}{4(nV_T)^2} = \frac{V_{RF}^2}{4nV_T} = \frac{R_0}{2nV_T} P_{RF} \quad (5)$$

By substituting the values we get a sensitivity between $0.5 \text{ mV}/\mu\text{W}$ and $1 \text{ mV}/\mu\text{W}$.

If we consider a noise floor equal to 100 nV , for example, the minimum RF input power is about -70 dBm , which is precisely the noise background of this type of detectors.

This discussion does not consider the non-ideality of the circuit and of the diode itself, and is mathematically valid only for input powers below -20 dBm , power level corresponding to the condition $V < V_T$.