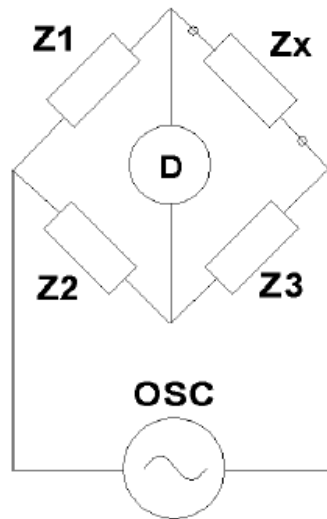


Radiofrequency Measurements

Impedance Measurements

Low-frequency Methods

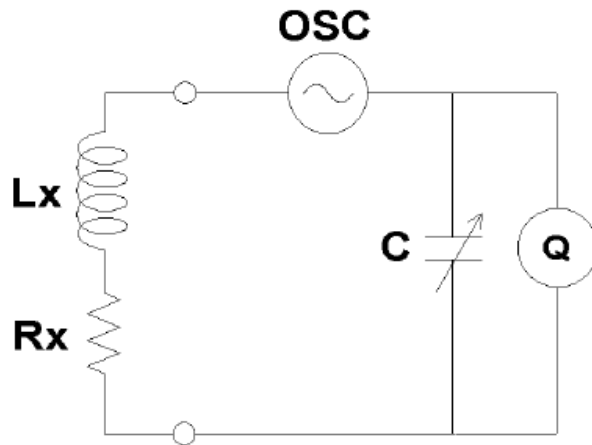
Bridge method



$$Z_x = \frac{Z_1}{Z_2} Z_3$$

When no current flows through the detector (D), the value of the unknown impedance Z_x can be obtained by the relationship of the other bridge elements. Various types of bridge circuits, employing combinations of L , C , and R components as the bridge elements, are used for various applications.

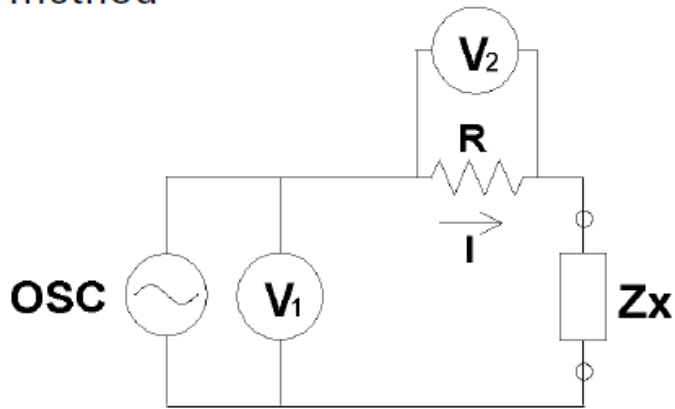
Resonant method



When a circuit is adjusted to resonance by adjusting a tuning capacitor C , the unknown impedance L_x and R_x values are obtained from the test frequency, C value, and Q value. Q is measured directly using a voltmeter placed across the tuning capacitor. Because the loss of the measurement circuit is very low, Q values as high as 1000 can be measured. Other than the direct connection shown here, series and parallel connections are available for a wide range of impedance measurements.

Low-frequency Methods

I-V method

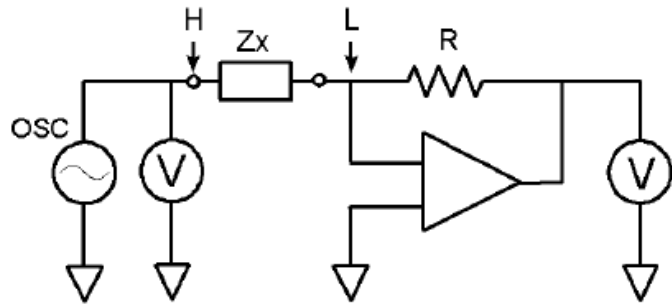


$$Z_x = \frac{V_1}{I} = \frac{V_1}{V_2} R$$

An unknown impedance Z_x can be calculated from measured voltage and current values. Current is calculated using the voltage measurement across an accurately known low value resistor, R . In practice a low-loss transformer is used in place of R to prevent the effects caused by placing a low value resistor in the circuit. The transformer, however, limits the low end of the applicable frequency range.

Low-frequency Methods

Auto balancing bridge method



The current, flowing through the DUT, also flows through resistor R . The potential at the “L” point is maintained at zero volts (thus called a “virtual ground”), because the current through R balances with the DUT current by operation of the I-V converter amplifier. The DUT impedance is calculated using voltage measurement at High terminal and that across R .

Note: In practice, the configuration of the auto balancing bridge differs for each type of instrument.

Generally LCR meters, in a low frequency range typically below 100 kHz, employ a simple operational amplifier for its I-V converter. This type of instrument has a disadvantage in accuracy, at high frequencies, because of performance limits of the amplifier. Wideband LCR meters and impedance analyzers employ the I-V converter consisting of sophisticated null detector, phase detector, integrator (loop filter) and vector modulator to ensure a high accuracy for a broad frequency range over 1 MHz. This type of instrument can attain to a maximum frequency of 110 MHz.

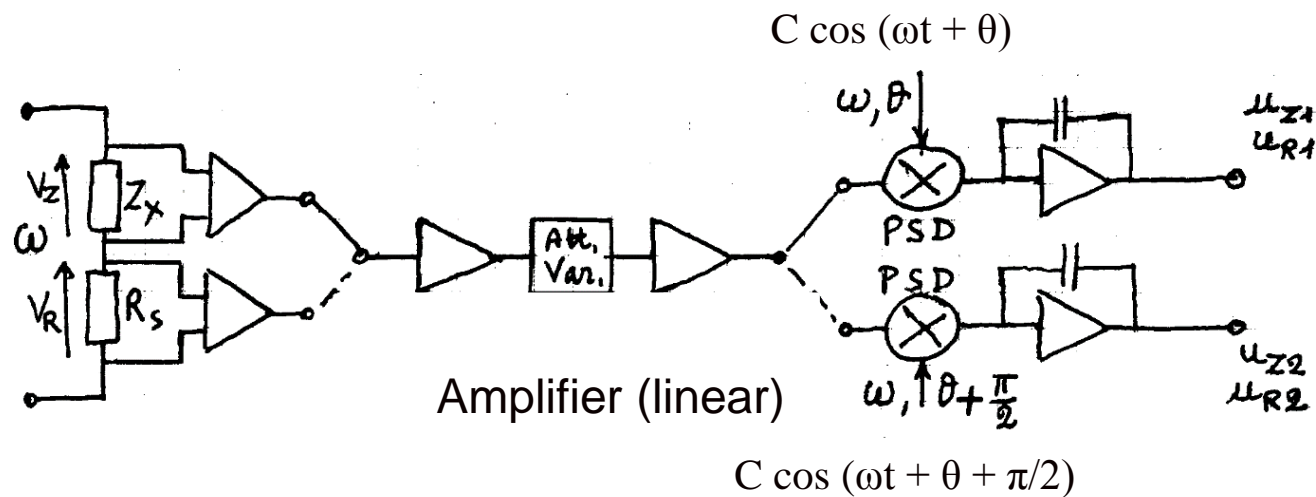
RF-IV

$$Z_X = |Z_X| e^{j\varphi}$$

$$V_Z = A \cos(\omega t + \varphi)$$

$$V_R = B \cos \omega t$$

$$\left| \frac{Z_X}{R_S} \right| = \frac{A}{B}$$



$$V = V_0 \cos(\omega t + \varphi) \cos(\omega t + \theta) = (V_0/2) [\cos(\varphi - \theta) + \cos(2\omega t + \varphi + \theta)]$$

$$\langle V \rangle = (V_0/2) \cos(\varphi - \theta)$$

$$u_{Z1} = kA \cos(\varphi - \theta)$$

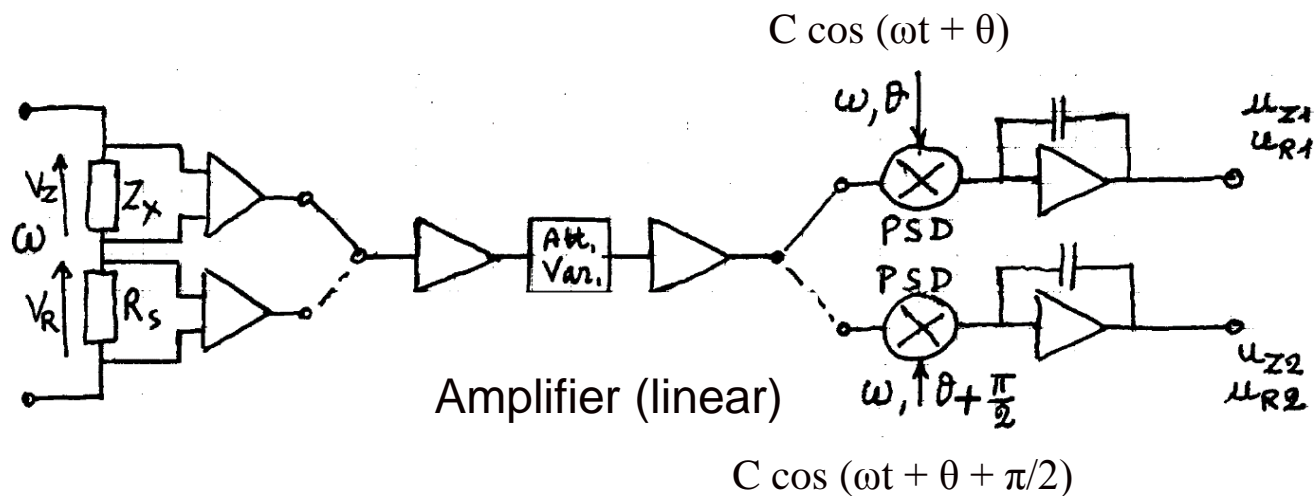
$$u_{Z2} = kA \cos(\varphi - \theta - \pi/2) = kA \sin(\varphi - \theta)$$

$$u_{R1} = kB \cos(-\theta)$$

$$u_{R2} = kB \cos(-\theta - \pi/2) = kB \sin(-\theta)$$

RF-IV

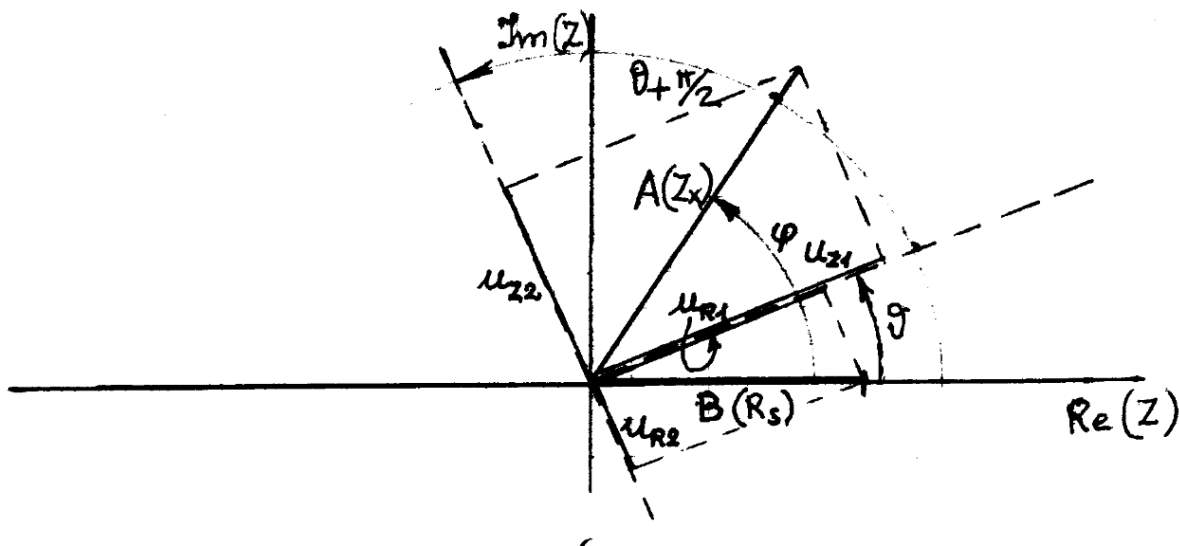
$$Z_X = |Z_X| e^{j\varphi}$$



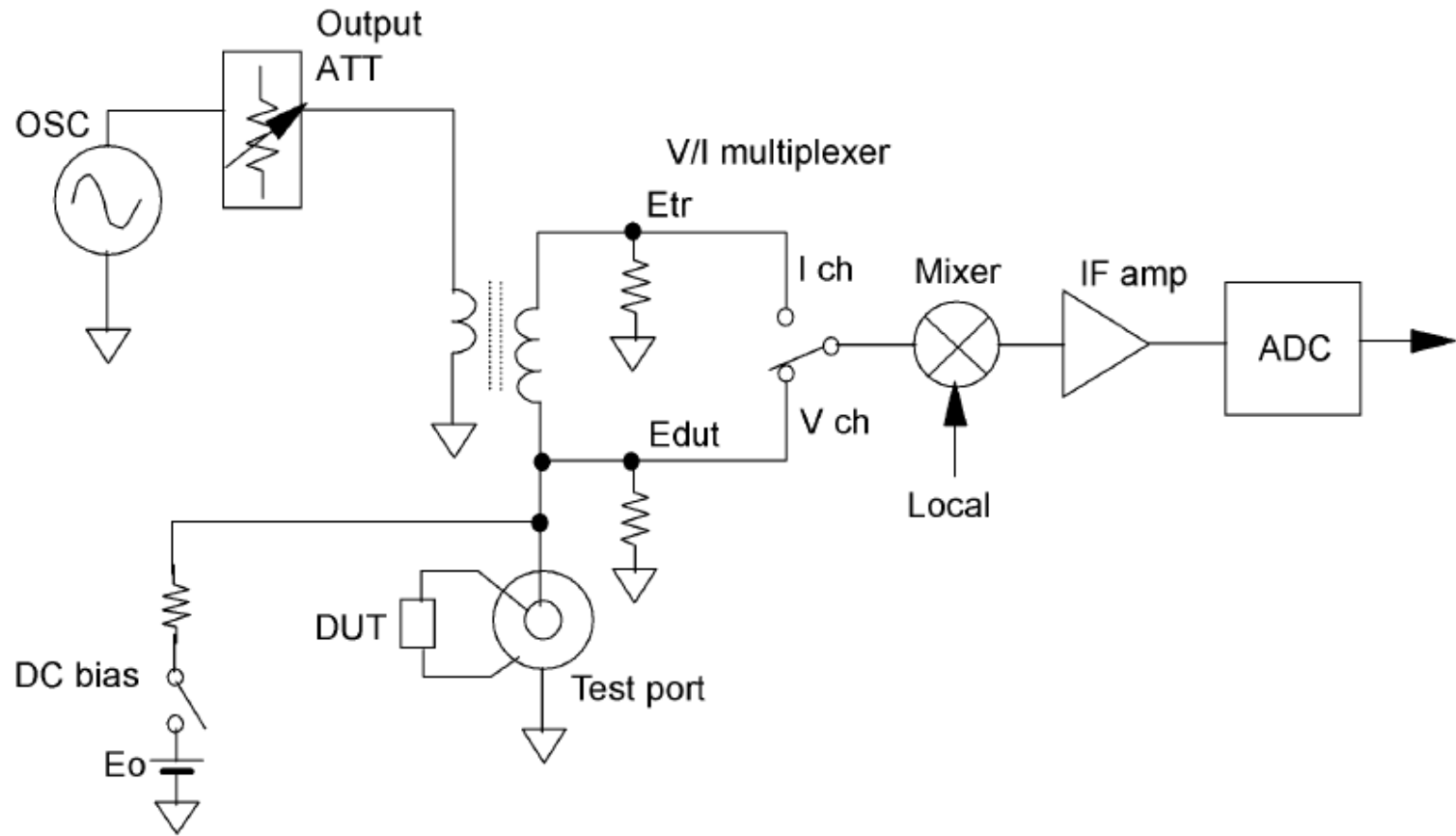
$$\left| \frac{Z_X}{R_S} \right| = \sqrt{\frac{u_{Z1}^2 + u_{Z2}^2}{u_{R1}^2 + u_{R2}^2}} = \frac{A}{B}$$

$$\cos \varphi = \frac{B}{A} \frac{u_{R1} u_{Z1} + u_{R2} u_{Z2}}{u_{R1}^2 + u_{R2}^2}$$

$$\sin \varphi = \frac{B}{A} \frac{u_{R1} u_{Z2} - u_{R2} u_{Z1}}{u_{R1}^2 + u_{R2}^2}$$

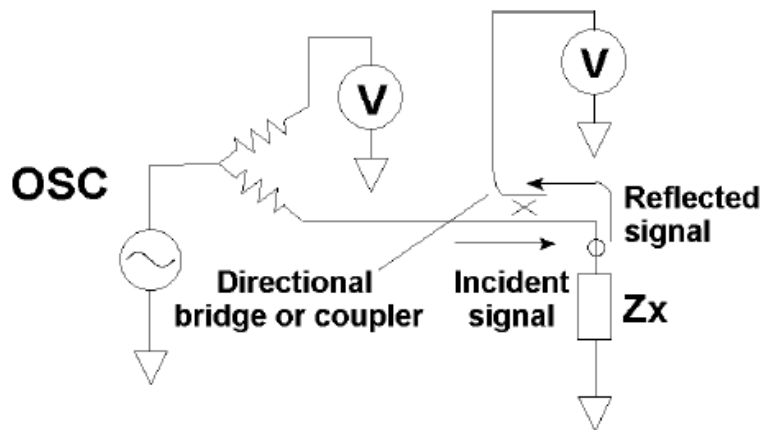


RF-IV (for GHz)



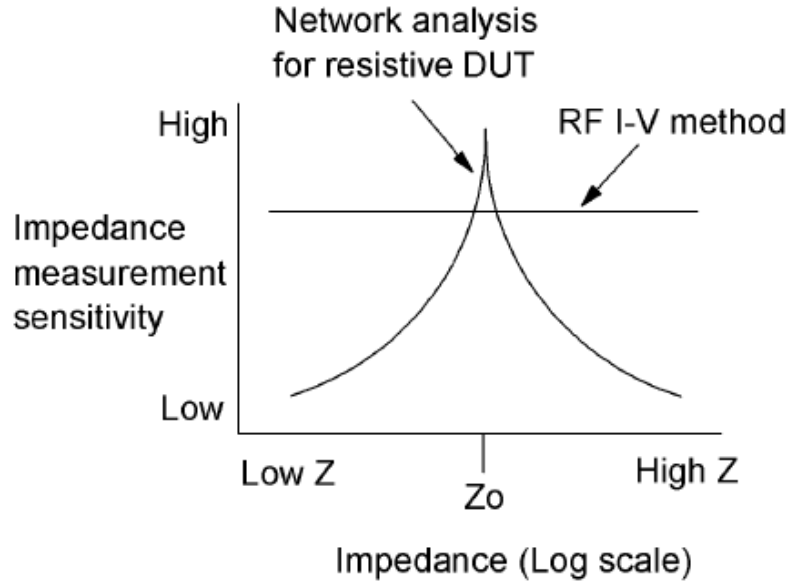
High-frequency Methods

Network analysis method

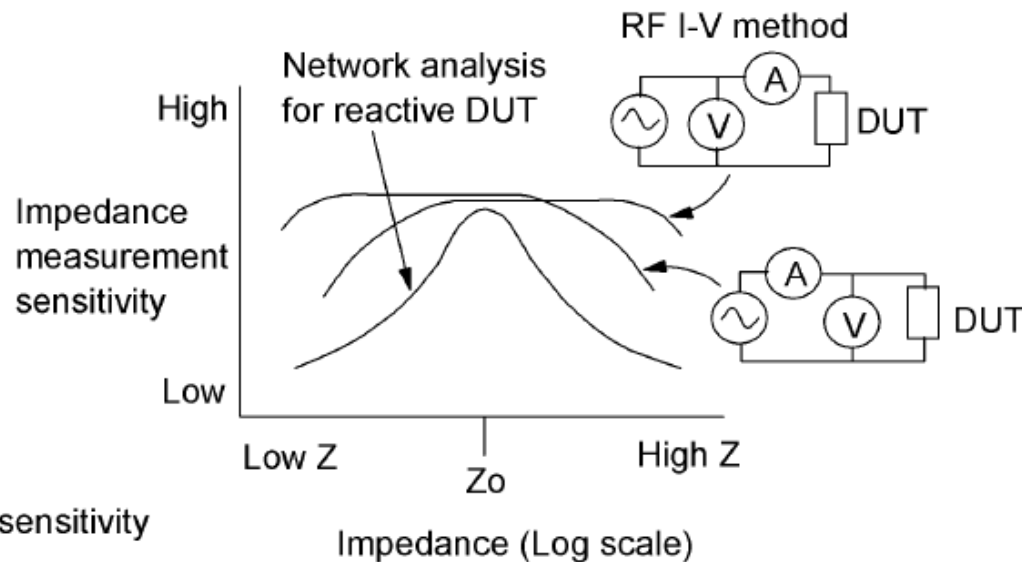
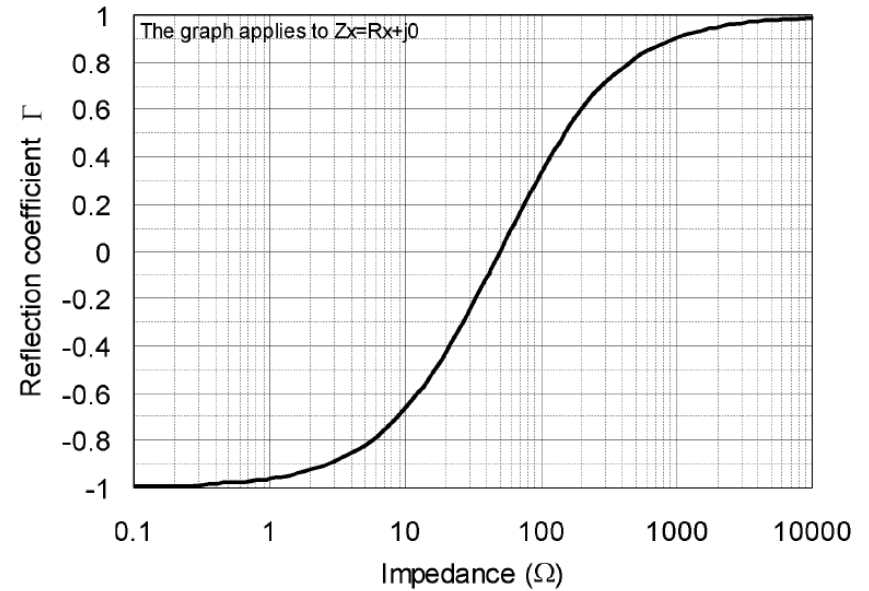


The reflection coefficient is obtained by measuring the ratio of an incident signal to the reflected signal. A directional coupler or bridge is used to detect the reflected signal and a network analyzer is used to supply and measure the signals. Since this method measures reflection at the DUT, it is usable in the higher frequency range.

High-frequency Methods

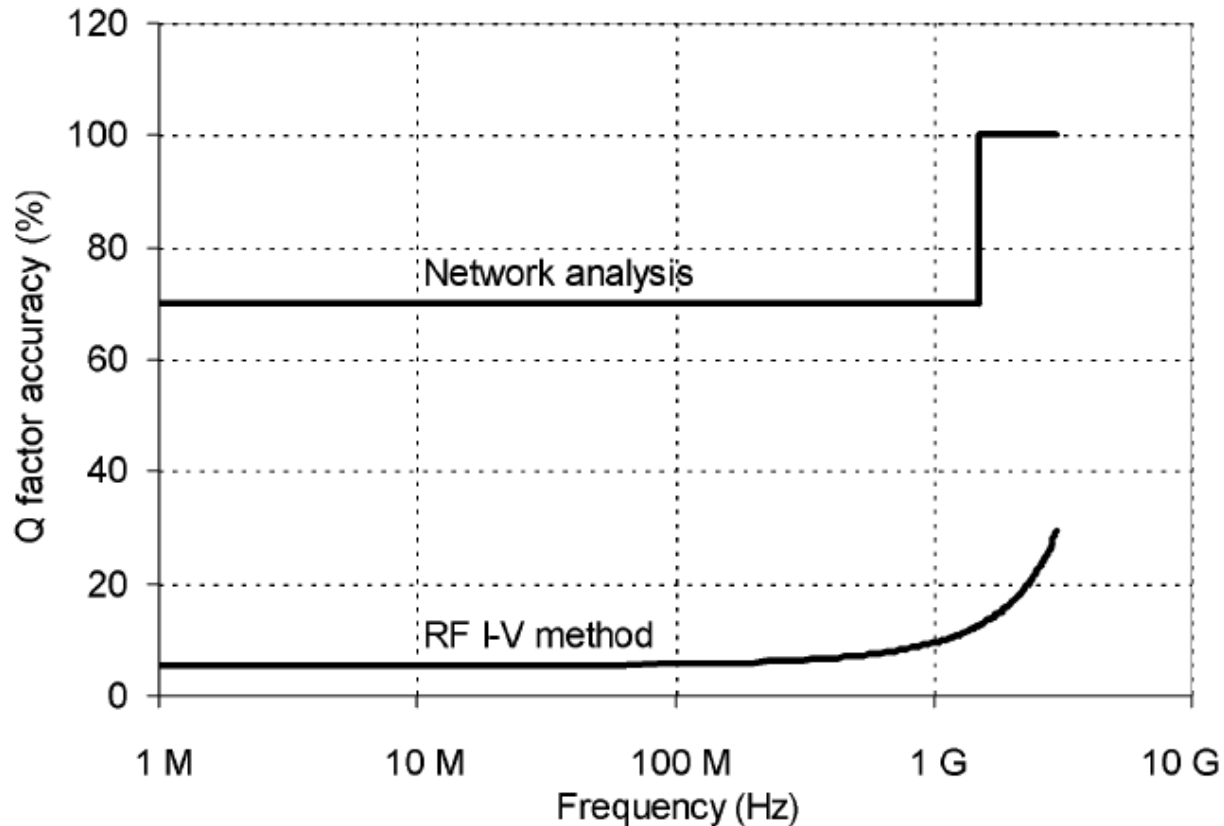


(a) Theoretical measurement sensitivity



(b) Practical measurement sensitivity

High-frequency Methods



Note: The Q accuracy is compared at Q factor of 100 at 50 Ω impedance.

Measurement Methods

| | Advantages | Disadvantages | Applicable frequency range | Typical Agilent products | Common application |
|------------------------------|---|--|----------------------------|--|---|
| Bridge method | High accuracy (0.1%typ.). Wide frequency coverage by using different types of bridges. Low cost. | Need to be manually balanced. Narrow frequency coverage with a single instrument. | DC to 300 MHz | None | Standard lab |
| Resonant method | Good Q accuracy up to high Q. | Need to be tuned to resonance. Low impedance measurement accuracy. | 10 kHz to 70 MHz | None | High Q device measurement. |
| I-V method | Grounded device measurement. Suitable to probe type test needs. | Operating frequency range is limited by transformer used in probe. | 10 kHz to 100 MHz | None | Grounded device measurement. |
| RF I-V method | High accuracy (1% typ.) and wide impedance range at high frequencies. | Operating frequency range is limited by transformer used in test head. | 1 MHz to 3 GHz | 4287A 4395A+43961A 4396B+43961A E4991A | RF component measurement. |
| Network analysis method | High frequency Range. Good accuracy when the unknown impedance is close to the characteristic impedance | Recalibration required when the measurement frequency is changed. Narrow impedance measurement range. | 300 kHz and above | 8753E 4395A | RF component measurement. |
| Auto balancing bridge method | Wide frequency coverage from LF to HF. High accuracy over a wide impedance measurement range. Grounded device measurement | Higher frequency ranges not available. | 20 Hz to 110 MHz | 4284A 4294A 4294A+42941A (*1) 4294A+42942A (*1) | Generic component measurement (*1) Grounded device measurement |